

## PERMALLOY MAGNETIZATION REVERSAL SENSOR

### TECHNICAL FIELD

5        [001] Embodiments are generally related to magnetic sensors. Embodiments are also related to magnetoresistive materials and magnetoresistive-based sensors. Embodiments are additionally related to permalloy materials and magnetic sensors which incorporate such permalloy materials.

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### BACKGROUND OF THE INVENTION

      [002] Magnetoresistors are often utilized for the contactless detection of changes in state, such as the measurement of an angular position of a  
15        rotatably mounted part. Magnetoresistive-based sensors typically include magnetic field-dependent resistors, which are arranged in a bridge circuit configuration and through which a control current is fed. When a magnetoresistive-based sensor is influenced by a magnetic field, a voltage can be established in which the magnitude of the voltage depends on the  
20        magnitude and direction of the magnetic field associated with the sensor.

      [003] The relationship between an associated bridge circuit voltage and the magnetic field direction can be utilized in a contactless magnetoresistive sensor, for example, to detect the angular position of a  
25        rotatably mounted part. Such sensors are particularly useful in automotive applications. Magnetoresistive sensors are typically configured from a magnetoresistive film that is formed from a magnetic substance that exhibits a magnetoresistive effect and generally possesses a single active layered structure.

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      [004] A magnetoresistive sensor may be acted upon by a magnetic field oriented in a particular manner, such that a definite control current can be applied to the current contacts of an associated bridge circuit. The

voltage that is then established at the other contacts can be measured on an ongoing basis. In general, the serpentine pattern of magnetoresistive material utilized in magnetoresistive sensors can be connected electrically in a Wheatstone bridge arrangement in order to sense changes in the resistance of the magnetoresistive material in response to changes in the strength and direction of a magnetic field component in the plane of the magnetoresistive elements. In order to monitor the changes in the resistance of the material, associated components, such as amplifiers, are generally connected together to form an electrical circuit, which provides an output signal that is representative of the strength and direction of the magnetic field in the plane of the sensing elements.

[005] When the circuit is provided on a silicon substrate, for example, electrical connections between associated components can be made above the surface of the silicon or by appropriately doped regions beneath the components and within the body of the silicon substrate. Components can be connected to each other above the surface of the silicon by disposing conductive material to form electrically conductive paths between the components. When appropriately doped regions within the silicon substrate connect components in electrical communication with each other, an electrically conductive path can be formed by diffusing a region of the silicon with an appropriate impurity, such as phosphorous, arsenic or boron to form electrically conductive connections between the components.

[006] Sensors may utilize an integrated coil that senses the magnetization flip of a single un-powered permalloy runner. Note that as utilized herein, the term "permalloy" generally refers to any of several alloys of nickel and iron having high magnetic permeability. Typical magnetoresistive devices utilize the small electrical resistance change of the permalloy film to a magnetic field by forcing a current through the runner and measuring the voltage change. This is often accomplished in a Wheatstone bridge configuration with many runners arranged electrically in series per

bridge element to maintain the current low and the sensitivity high.

[007] Based on the foregoing, it would therefore be advantageous to produce a magnetic sensor that exhibits a high sensitivity, low current, and  
5 which is small and inexpensive. It would also be advantageous to produce a magnetic sensor which does not rely on many runners per bridge element, but utilizes a minimum number of permalloy runners, and in particular, which do not require an electrical current for operations thereof. It is believed that if such a configuration can be effectively produced; magnetic sensors can be  
10 implemented which are much more compact and efficient than present magnetic sensors.

## BRIEF SUMMARY OF THE INVENTION

5 [008] The following summary of the invention is provided to facilitate an understanding of some of the innovative features unique to the present invention and is not intended to be a full description. A full appreciation of the various aspects of the invention can be gained by taking the entire specification, claims, drawings, and abstract as a whole.

10 [009] It is, therefore, one aspect of the present invention to provide an improved magnetic sensor.

[0010] It is another aspect of the present invention to provide for an improved magnetoresistive sensor.

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[0011] It is yet a further aspect of the present invention to provide for a permalloy magnetic sensor.

20 [0012] It is an additional aspect of the present invention to provide for a permalloy magnetic sensor, which utilizes at a minimum, only one permalloy runner and does not require a current for operations thereof. The aforementioned aspects of the invention and other objectives and advantages can now be achieved as described herein. A magnetic sensor is disclosed in which a ferromagnetic runner (e.g., a permalloy runner) can be  
25 located relative to a target. A coil structure can be generally wound about the ferromagnetic runner, such that when a magnetic field changes direction along an axial length of the ferromagnetic runner (e.g., above a certain level,  $H_c$ ), a voltage is induced in the coil structure that is proportional to a time range of change of a magnetic flux thereof.

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[0013] Additionally, an interfacing circuit can be provided, wherein the ferromagnetic runner and the coil structure are integrated with the interfacing

circuit to thereby produce a magnetic sensor for magnetically sensing the target, wherein the magnetic sensor is highly sensitive and operates upon a negligible electrical current. The coil structure itself can be wound tightly about the ferromagnetic runner, such that the coil structure possesses a  
5 number of turns thereof, which is sufficient to achieve a voltage spike amplitude for the interfacing circuit induced therein when the magnetic field causes the internal magnetization to change direction along the axial length of the ferromagnetic runner.

10 [0014] The ferromagnetic runner and the coil can also be integrated with the interfacing circuit utilizing either levels of interconnecting metal or a conductive semiconductor layer for the coil structure, such that the conductive semiconductor layer is located between the ferromagnetic runner and an insulating above. The voltage induced in the coil structure is  
15 equivalent to a number of turns of the coil structure multiplied by a cross sectional area of the ferromagnetic runner multiplied by a rate of change of magnetic flux density with respect to a change of time. Additionally, a single device can provide speed and direction information.

## BRIEF DESCRIPTION OF THE DRAWINGS

[0015] The accompanying figures, in which like reference numerals  
5 refer to identical or functionally-similar elements throughout the separate  
views and which are incorporated in and form a part of the specification,  
further illustrate the present invention and, together with the detailed  
description of the invention, serve to explain the principles of the present  
invention.

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[0016] FIG. 1 illustrates a permalloy runner having a magnetization  
direction along an axial length, in accordance with a preferred embodiment  
of the present invention;

15 [0017] FIG. 2 illustrates the permalloy runner of FIG. 1 having a  
reverse magnetization direction along the axial length thereof, in accordance  
with a preferred embodiment of the present invention;

[0018] FIG. 3 illustrates the permalloy runner of FIGS. 1-2 having a  
20 wound coil thereof, in accordance with a preferred embodiment of the  
present invention;

[0019] FIG. 4 illustrates a graph of output voltage versus applied field  
for the permalloy runner depicted in FIGS. 1-3 herein, in accordance with a  
25 preferred embodiment of the present invention; and

[0020] FIG. 5 illustrates a block diagram of a configuration in which an  
interfacing circuit is adapted for use with a ferromagnetic runner and a coil  
structure, in accordance with an alternative embodiment of the present  
30 invention.

## DETAILED DESCRIPTION OF THE INVENTION

[0021] The particular values and configurations discussed in these  
5 non-limiting examples can be varied and are cited merely to illustrate at  
least one embodiment of the present invention and are not intended to limit  
the scope of the invention.

[0022] FIG. 1 illustrates a permalloy runner 100 having a  
10 magnetization direction along an axial length, in accordance with a preferred  
embodiment of the present invention. FIG. 2 illustrates the permalloy runner  
100 of FIG. 1 having a reverse magnetization direction along the axial length  
thereof, in accordance with a preferred embodiment of the present invention.

FIG. 3 illustrates the permalloy runner 100 of FIGS. 1-2 having a wound coil  
15 thereof, in accordance with a preferred embodiment of the present invention.

Note that in FIGS. 1-3, like or analogous parts are generally indicated by  
identical reference numerals.

[0023] As indicated in FIG. 3, a single coil 304 can be wound about  
20 the permalloy runner 100, such that when a magnetic field changes direction  
along an axial length of the permalloy runner, as indicated by arrow 102 of  
FIG. 1 and arrow 104 of Fig. 4, a voltage,  $V$ , is induced in the coil that 304 is  
proportional to a time rate of change of a magnetic flux thereof. Voltage  $V$  is  
shown in FIG. 3. An interfacing circuit can be implemented in which the  
25 permalloy runner 100 and the coil 304 are integrated to thereby produce a  
magnetic sensor for magnetically sensing a target, wherein the magnetic  
sensor is highly sensitive and operates upon a negligible electrical current.

[0024] Additionally, a plurality of interconnecting metals 306 and 308  
30 can be utilized to integrate the permalloy runner 100 and the coil 304 with  
the interfacing circuit. When a magnetic field changes direction in the axis of  
the permalloy runner 100 length, the sudden magnetization reversal (i.e., see

arrows 102 and 104) induces a voltage in the surrounding coil 304 that is proportional to the time rate of change of the magnetic flux linking the interfacing circuit. Coil 304 can be tightly wound about the permalloy runner 100 with a sufficient number of turns to obtain the required voltage spike  
5 amplitude for the interfacing circuit.

[0025] The permalloy runner 100 and the coil 304 can be integrated with the interfacing circuit using either multiple levels of interconnecting metal such as interconnecting metal 306 and 308, or utilizing a conductive  
10 semiconductor layer such as a sinker resistor for coil structure beneath the permalloy runner 100 and insulated metal located above the permalloy runner. Interconnecting metal 306 of FIG. 3 refers generally to coil interconnecting metal located above permalloy runner 100, while interconnecting metal 308 refers to interconnecting metal (or semiconductor  
15 layers) located below permalloy runner 100. The configuration illustrated with respect to FIGS. 1-3 generally utilizes only one coil structure and only one ferromagnetic cell (i.e., permalloy runner 100) component based on the shape anisotropy of the ferromagnetic cell.

[0026] FIG. 4 illustrates a graph 400 of output voltage versus applied field for the permalloy runner depicted in FIGS. 1-3 herein, in accordance with a preferred embodiment of the present invention. Graph 400 can be produced based on equation (1) below, which is based on determining voltage V depicted in FIG. 3. The voltage V induced in the single coil 304 is  
20 generally equivalent to the number of turns of the coil multiplied by a cross sectional area of the permalloy runner 304 multiplied by a rate of change of magnetic flux with respect to a change of time.

$$V = n \cdot A \cdot dB/dT \quad (1)$$

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[0027] In calculating voltage V of equation (a), the variable N is equivalent to the number of turns of coil 304, and the variable A represents



the cross-sectional area of the permalloy runner 304. The variable  $B$  represents flux density, while the variable  $H$  represents flux, while the variable  $H_c$  represents the flux chirp. The formulation  $dB/dT$  represents the rate of change of the magnetic flux linking the interfacing circuit with respect  
5 to change in time.

[0028] It is important to note that the permalloy material itself can exhibit a “snapping action”, that once the field crosses through 0 Gauss, to a particular level (e.g.,  $H_c$  = flux chirp), the magnetization quickly “snaps” to the  
10 opposite direction. This snapping or chirping occurs extremely fast, on the order of nano seconds. Thus,  $dB$  is small, and  $dt$  is very small, so  $dB/dT$  is very large, and thus the voltage (i.e., calculated via equation 1 above) is large.

[0029] Because the magnetization can chirp in either direction ( $dB$  will be either sign), the voltage can be positive and negative. This feature can provide the direction of the magnetic field change. The resistance of permalloy is an even function (i.e., it does not “know” direction), so a single device based on conventional configurations will not provide both speed and  
20 direction information. Normally, two bridges would need to be placed in such a configuration physically offset to provide speed and direction information. The embodiments described herein, however, do not require the placement of two bridges in this manner. Due to the short time duration of the magnetization flip described herein, however, the magnetic sensor described  
25 herein is highly sensitive and can operate without electrical current or upon a negligible electrical current.

[0030] FIG. 5 illustrates a block diagram of a configuration 500 in which an interfacing circuit 504 is adapted for use with a ferromagnetic  
30 runner 502 and a coil structure 506, in accordance with an alternative embodiment of the present invention. Note that ferromagnetic runner 502 can be implemented as a permalloy runner such as, for example, permalloy

runner 100 depicted in FIGS. 1-3. Similarly, coil structure 506 can be implemented as a coil structure such as, for example, coil 304 described herein.

5           [0031] Thus, ferromagnetic runner 502 can be located relative to a target (not shown in FIG. 5), and the coil structure 506 wound about the ferromagnetic runner 502, such that when a magnetic field changes direction along an axial length of the ferromagnetic runner 502, a voltage is induced in the coil structure 506 that is proportional to a time range of change of a  
10 magnetic flux thereof. The interfacing circuit 502 functions to interface the ferromagnetic runner 502 and the coil structure 506, wherein the ferromagnetic runner 502 and the coil structure 506 are integrated with the interfacing circuit 504 to thereby produce a magnetic sensor for magnetically sensing the target.

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          [0032] Several advantages can be obtained by implementing embodiments of the present invention within the context of a magnetic sensor configuration. For example, embodiments generally rely upon the magnetization reversal phenomenon in a manner that eliminates hysteresis  
20 components in associated magnetic sensor integrated circuits, which in turn can also lower the overall current required by such integrated circuits. Note that as utilized herein, the term "hysteresis" refers generally to the lagging of an effect behind its cause. Another advantage of the present invention stems from the fact the magnetic sensor described herein does not require  
25 the use of many ferromagnetic cells to measure the direction of magnetization.

          [0033] The embodiments and examples set forth herein are presented to best explain the present invention and its practical application and to  
30 thereby enable those skilled in the art to make and utilize the invention. Those skilled in the art, however, will recognize that the foregoing description and examples have been presented for the purpose of illustration and

example only. Other variations and modifications of the present invention will be apparent to those of skill in the art, and it is the intent of the appended claims that such variations and modifications be covered.

5           [0034] The description as set forth is not intended to be exhaustive or  
to limit the scope of the invention. Many modifications and variations are  
possible in light of the above teaching without departing from the scope of  
the following claims. It is contemplated that the use of the present invention  
can involve components having different characteristics. It is intended that  
10 the scope of the present invention be defined by the claims appended hereto,  
giving full cognizance to equivalents in all respects.